

Figure B.24 - Example of banjir bandang hazard map on kali Jompo catchment area after updated by using field survey data



Figure B.25 - Example of risk map of banjir bandang



Figure B.26 – Method of defining topographic slope of river segment



Figure B.27 – Method to making banjir bandang prone areas manually



Figure B.28 – Handheld GPS



Figure B.29 – Clinometer



Figure B.30 – Compasses



Figure B.31 – Disto/ digital measurement tool

### Appendix C (informative) Table

# Table C.1 – The types of imagery data and its feature

| Imagery                                       | Feature   | Price estimation  |
|---|---|---|
| ALOS (Advanced Land<br>Observation Satellite) | <ul> <li>ALOS PRISM <ul> <li>Black n White</li> <li>Spatial resolution = 2,5 m</li> <li>Coverage area 70 km x 35 km (1 scene)</li> </ul> </li> <li>ALOS AVNIR-2 <ul> <li>Color</li> <li>Spatial resolution = 10 m</li> <li>Coverage area 70 km x 60 km (1 scene)</li> </ul> </li> </ul>   | <ul> <li>For archive data:</li> <li>Full scene (70 km x 35 km), resolution 2.5m B/W = Rp 4.500.000</li> <li>Full scene (70 km x 60 km), resolution 10m color = Rp 5.000.000</li> <li>Full scene (70 km x 60 km), resolution 2.5m color = Rp 12.500.000</li> </ul>                     |
| SPOT  | <ul> <li>SPOT 5 <ul> <li>Color and Black n White</li> <li>Spatial resolution = 2,5 m, 5 m, 10 m</li> <li>Coverage area 60 km x 60 km (1 scene)</li> </ul> </li> <li>SPOT 4 <ul> <li>Color and Black n White</li> <li>Spatial resolution = 10 m, 20 m</li> <li>Coverage area 60 km x 60 km (1 scene)</li> </ul> </li> <li>SPOT 1, 2, 3 <ul> <li>Color and Black n White</li> <li>Spatial resolution = 10 m, 20 m</li> <li>Coverage area 60 km x 60 km (1 scene)</li> </ul> </li> </ul> | <ul> <li>For SPOT 5.</li> <li>1/8 scene (441 km<sup>2</sup>), resolution 2.5m color<br/>= Rp 33.300.000</li> <li>1/8 scene (441 km<sup>2</sup>), resolution 5m color =<br/>Rp 23.670.000</li> <li>1/8 scene (441 km<sup>2</sup>), resolution 10m color =<br/>Rp 13.050.000</li> </ul> |
| IKONOS  | <ul> <li>Color</li> <li>Spatial resolution = 1 m.</li> <li>The area of minimum purchase = 100 km<sup>2</sup></li> </ul>   | <ul> <li>Minimum purchase 100km<sup>2</sup>.</li> <li>Archive data, 12 – 30 USD / km<sup>2</sup>.</li> <li>New acquisition, 20 – 35 USD / km<sup>2</sup>.</li> </ul>  |
| Quickbird                                     | <ul> <li>Color</li> <li>Spatial resolution = 0,65 m</li> </ul>  | <ul> <li>Minimum purchase of archive = 25km<sup>2</sup>,</li> <li>Minimum purchase of new acquisition = 90km<sup>2</sup>.</li> <li>Archive data, 14 USD / km<sup>2</sup>.</li> <li>New acquisition, 17 USD / km<sup>2</sup>.</li> </ul>   |
| World View                                    | <ul> <li>WorldView-2 &amp; WorldView-1</li> <li>Color</li> <li>Spatial resolution = 0,5 m</li> <li>The area of minimum purchase = 25 km<sup>2</sup></li> </ul>  | <ul> <li>Minimum purchase of archive = 25km<sup>2</sup>,</li> <li>Minimum purchase of new acquisition = 90km<sup>2</sup>.</li> <li>Archive data, 14 USD / km<sup>2</sup>.</li> <li>New acquisition, 17 USD / km<sup>2</sup>.</li> </ul>   |
| Aerial Photographs                            | <ul> <li>Color</li> <li>Cloud-free</li> <li>Spatial resolution ≈ 0,3 m</li> </ul>   |   |

# Table C.2 - Information table about the intersection between sub-area and landslide area

| Sub-<br>area ID | Landslide<br>occurrence per sub-<br>area | Landslide potential based on<br>past landslide events |  |  |  |  |
|-----------------|--|---|--|--|--|--|
|                 |  |   |  |  |  |  |
| 95              | 0  | 0   |  |  |  |  |
| 96              | 0  | 0   |  |  |  |  |
| 97              | 0  | 0   |  |  |  |  |
| 98              | 2  | 1   |  |  |  |  |
| 99              | 1  | 1   |  |  |  |  |
| 100             | 0  | 0   |  |  |  |  |
| 101             | 3  | 1   |  |  |  |  |
| 102             | 0  | 0   |  |  |  |  |
| 103             | 0  | 0   |  |  |  |  |
| 104             | 0  | 0   |  |  |  |  |
| 105             | 0  | 0   |  |  |  |  |

| 106 | 0 | 0 |
|-----|---|---|
| 107 | 0 | 0 |
| 108 | 0 | 0 |
|     |   |   |

# Table C.3 - Information table about the intersection between sub-areas and geological or micro-topographic elements

| Past land       | slide per sub-<br>area  |             | Geological and micro-topographic elements |             |                      |             |                      |  |
|-----------------|-------------------------|-------------|---|-------------|----------------------|-------------|----------------------|--|
| Sub-<br>area ID | Landslide<br>occurrence | Sub-area ID | Landslide occurrence                      | Sub-area ID | Landslide occurrence | Sub-area ID | Landslide occurrence |  |
|                 |                         |             |   |             |                      |             |                      |  |
| 400             | 1                       | 0           | 0   | 0           | 0                    | 0           | 0                    |  |
| 401             | 0                       | 0           | 0   | 0           | 0                    | 0           | 0                    |  |
| 402             | 0                       | 0           | 0   | 0           | 0                    | 0           | 0                    |  |
| 403             | 0                       | 0           | 0   | 0           | 1                    | 1           | 0                    |  |
| 404             | 0                       | 0           | 0   | 0           | 0                    | 0           | 0                    |  |
| 405             | 0                       | 0           | 0   | 0           | 0                    | 0           | 0                    |  |
| 406             | 1                       | 0           | 0   | 0           | 0                    | 0           | 0                    |  |
| 407             | 1                       | 0           | 0   | 0           | 0                    | 0           | 0                    |  |
| 408             | 0                       | 0           | 0   | 0           | 0                    | 0           | 0                    |  |
| 409             | 0                       | 0           | 0   | 0           | 0                    | 0           | 0                    |  |
| 410             | 1                       | 0           | 0   | 0           | 0                    | 0           | 0                    |  |
| 411             | 0                       | 0           | 0   | 0           | 0                    | 0           | 0                    |  |
| 412             | 0                       | 0           | 0   | 0           | 0                    | 0           | 0                    |  |
| 413             | 0                       | 0           | 0   | 0           | 0                    | 0           | 0                    |  |
| 414             | 0                       | 0           | 0   | 0           | 0                    | 0           | 0                    |  |
| 415             | 0                       | 0           | 0   | 0           | 0                    | 0           | 0                    |  |
| 416             | 0                       | 0           | 0   | 0           | 0                    | 0           | 0                    |  |
| 417             | 0                       | 0           | 0   | 0           | 0                    | 0           | 0                    |  |
| 418             | 0                       | 0           | 0   | 0           | 1                    | 1           | 0                    |  |
|                 |                         |             |   |             |                      |             |                      |  |

# Table C.4 – Information table of finding the best combination of geological/microtopographic elements

| Sub-<br>area ID | Landslide<br>events | Circular arc crack<br>(A) |    | Ancien<br>seated l<br>(I | t deep-<br>andslide<br>3) | A and B |    | Ac | or B |
|-----------------|---------------------|---------------------------|----|--------------------------|---------------------------|---------|----|----|------|
|                 |                     | S3                        | S2 | S3                       | S2                        | S3      | S2 | S3 | S2   |
|                 |                     |                           |    |                          |                           |         |    |    |      |
| 400             | 1                   | 0                         | 0  | 0                        | 0                         | 0       | 0  | 0  | 0    |
| 401             | 0                   | 0                         | 0  | 0                        | 0                         | 0       | 0  | 0  | 0    |
| 402             | 0                   | 0                         | 0  | 0                        | 0                         | 0       | 0  | 0  | 0    |
| 403             | 0                   | 0                         | 0  | 0                        | 0                         | 0       | 0  | 0  | 0    |
| 404             | 0                   | 0                         | 0  | 1                        | 0                         | 0       | 0  | 1  | 0    |
| 405             | 0                   | 0                         | 0  | 1                        | 0                         | 0       | 0  | 1  | 0    |
| 406             | 1                   | 0                         | 0  | 0                        | 0                         | 0       | 0  | 0  | 0    |
| 407             | 1                   | 0                         | 0  | 1                        | 1                         | 0       | 0  | 1  | 1    |
| 408             | 0                   | 1                         | 0  | 1                        | 0                         | 1       | 0  | 1  | 0    |
| 409             | 0                   | 0                         | 0  | 0                        | 0                         | 0       | 0  | 0  | 0    |
| 410             | 1                   | 0                         | 0  | 0                        | 0                         | 0       | 0  | 0  | 0    |
| 411             | 0                   | 0                         | 0  | 1                        | 0                         | 0       | 0  | 1  | 0    |
| 412             | 0                   | 0                         | 0  | 1                        | 0                         | 0       | 0  | 1  | 0    |
| 413             | 0                   | 0                         | 0  | 0                        | 0                         | 0       | 0  | 0  | 0    |
| 414             | 0                   | 0                         | 0  | 0                        | 0                         | 0       | 0  | 0  | 0    |
| 415             | 0                   | 0                         | 0  | 0                        | 0                         | 0       | 0  | 0  | 0    |
| 416             | 0                   | 0                         | 0  | 0                        | 0                         | 0       | 0  | 0  | 0    |
| 417             | 0                   | 0                         | 0  | 0                        | 0                         | 0       | 0  | 0  | 0    |
| 418             | 0                   | 0                         | 0  | 0                        | 0                         | 0       | 0  | 0  | 0    |
|                 |                     |                           |    |                          |                           |         |    |    |      |

| Points<br>ID | Pixel wide | Slope | Accumulation<br>value | Pixel wide x<br>accumulation<br>flow value | log(pixel wide x<br>accumulation<br>flow value) |
|--------------|------------|-------|-----------------------|--|---|
| 52070        | 2500       | 14.13 | 0                     | 0  | 0.00  |
| 52071        | 2500       | 12.31 | 0                     | 0  | 0.00  |
| 52072        | 2500       | 13.50 | 13                    | 32500                                      | 4.51  |
| 52073        | 2500       | 14.62 | 20                    | 50000                                      | 4.70  |
| 52074        | 2500       | 13.84 | 0                     | 0  | 0.00  |
| 52075        | 2500       | 15.25 | 2                     | 5000                                       | 3.70  |
| 52076        | 2500       | 18.02 | 0                     | 0  | 0.00  |
| 52077        | 2500       | 19.01 | 0                     | 0  | 0.00  |
| 52078        | 2500       | 37.12 | 0                     | 0  | 0.00  |
|              |            |       |                       |  |   |

### Table C.5 - Example of extraction results data table of point attribute data to calculate the value log(pixel wide x accumulation flow value)

#### Table C.6 - Example of data table to calculate amount of points that match the range criteria of slope value and the value of log(pixel wide x accumulation flow value) which from all of study area

| slope   | 3.4 - 3.7 | 3.7 - 3.88 | 3.88 - 4.1 | 4.1 - 4.44 | 4.44 -<br>4.72 | 4.72 -<br>5.11 | 5.11 - 5.4 | 5.4 - 5.7             | 5.7 <  |
|---------|-----------|------------|------------|------------|----------------|----------------|------------|-----------------------|--------|
| 0 - 10  | 6281      | 3516       | 3768       | 4510       | 2896           | 3297           | 2202       | 2166                  | 7169   |
| 10 - 15 | 6623      | 3472       | 3459       | 3497       | 1906           | 1890           | 1191       | 1116                  | 1940   |
| 15 - 20 | 7214      | 3482       | 3069       | 2956       | 1399           | 1249           | 712        | 563                   | 948    |
| 20 - 25 | 6380      | 3117       | 2509       | 2258       | 1028           | 885            | 410        | 309                   | 446    |
| 25 - 30 | 5287      | 2643       | 2211       | 1926       | 747            | 540            | 246        | 132                   | 226    |
| 30 - 35 | 4568      | 2347       | 1858       | 1396       | 536            | 363            | 133        | 83                    | 114    |
| 35 - 40 | 3332      | 1709       | 1366       | 1026       | 299            | 208            | 84         | 38                    | 52     |
| 40 <    | 4096      | 2397       | 2100       | 1609       | 511            | 310            | 97         | 28                    | 63     |
|         |           |            |            |            |                |                | 1          | otal points<br>number | 144514 |

#### Table C.7 - Example of data table to calculate amount of points that match the range criteria of slope value and the value of log(pixel wide x accumulation flow value) which intersect to landslide area

| slope   | 3.4 - 3.7 | 3.7 - 3.88 | 3.88 - 4.1 | 4.1 - 4.44 | 4.44 -<br>4.72 | 4.72 -<br>5.11 | 5.11 - 5.4 | 5.4 - 5.7 | 5.7 < |
|---------|-----------|------------|------------|------------|----------------|----------------|------------|-----------|-------|
| 0 - 10  | 2         | 1          | 0          | 0          | 0              | 3              | 1          | 0         | 9     |
| 10 - 15 | 1         | 3          | 2          | 3          | 6              | 4              | 3          | 1         | 4     |
| 15 - 20 | 9         | 4          | 11         | 11         | 10             | 6              | 3          | 0         | 5     |
| 20 - 25 | 10        | 12         | 11         | 19         | 5              | 3              | 0          | 1         | 3     |
| 25 - 30 | 12        | 18         | 14         | 19         | 5              | 3              | 0          | 0         | 3     |
| 30 - 35 | 31        | 13         | 10         | 13         | 3              | 3              | 2          | 0         | 0     |
| 35 - 40 | 19        | 16         | 9          | 6          | 3              | 2              | 0          | 0         | 0     |
| 40 <    | 77        | 51         | 38         | 43         | 25             | 4              | 1          | 0         | 1     |
|         |           |            |            |            |                |                | Total poin | ts number | 610   |

| slope   | 3.4 - 3.7 | 3.7 - 3.88 | 3.88 - 4.1 | 4.1 - 4.44 | 4.44 -<br>4.72 | 4.72 -<br>5.11 | 5.11 - 5.4 | 5.4 - 5.7        | 5.7 < |
|---------|-----------|------------|------------|------------|----------------|----------------|------------|------------------|-------|
| 0 - 10  | 0.000     | 0.000      | 0.000      | 0.000      | 0.000          | 0.001          | 0.000      | 0.000            | 0.001 |
| 10 - 15 | 0.000     | 0.001      | 0.001      | 0.001      | 0.003          | 0.002          | 0.003      | 0.001            | 0.002 |
| 15 - 20 | 0.001     | 0.001      | 0.004      | 0.004      | 0.007          | 0.005          | 0.004      | 0.000            | 0.005 |
| 20 - 25 | 0.002     | 0.004      | 0.004      | 0.008      | 0.005          | 0.003          | 0.000      | 0.003            | 0.007 |
| 25 - 30 | 0.002     | 0.007      | 0.006      | 0.010      | 0.007          | 0.006          | 0.000      | 0.000            | 0.013 |
| 30 - 35 | 0.007     | 0.006      | 0.005      | 0.009      | 0.006          | 0.008          | 0.015      | 0.000            | 0.000 |
| 35 - 40 | 0.006     | 0.009      | 0.007      | 0.006      | 0.010          | 0.010          | 0.000      | 0.000            | 0.000 |
| 40 <    | 0.019     | 0.021      | 0.018      | 0.027      | 0.049          | 0.013          | 0.010      | 0.000            | 0.016 |
|         |           |            |            |            |                |                |            | Average<br>ratio | 0.004 |

# Table C.9 - Selecting cell that has the same or more than twice value than the average ratio value

| slope   | 3.4 - 3.7 | 3.7 - 3.88 | 3.88 - 4.1 | 4.1 - 4.44 | 4.44 -<br>4.72 | 4.72 -<br>5.11 | 5.11 - 5.4 | 5.4 - 5.7 | 5.7 < |
|---------|-----------|------------|------------|------------|----------------|----------------|------------|-----------|-------|
| 0 - 10  | 0.075     | 0.067      | 0.000      | 0.000      | 0.000          | 0.216          | 0.108      | 0.000     | 0.297 |
| 10 - 15 | 0.036     | 0.205      | 0.137      | 0.203      | 0.746          | 0.501          | 0.597      | 0.212     | 0.488 |
| 15 - 20 | 0.296     | 0.272      | 0.849      | 0.882      | 1.693          | 1.138          | 0.998      | 0.000     | 1.250 |
| 20 - 25 | 0.371     | 0.912      | 1.039      | 1.993      | 1.152          | 0.803          | 0.000      | 0.767     | 1.594 |
| 25 - 30 | 0.538     | 1.613      | 1.500      | 2.337      | 1,386          | 1.316          | 0.000      | 0.000     | 3.145 |
| 30 - 35 | 1.608     | 1.312      | 1.275      | 2.206      | 1.326          | 1.958          | 3.563      | 0.000     | 0.000 |
| 35 - 40 | 1.351     | 2.218      | 1.561      | 1.385      | 2.377          | 2.278          | 0.000      | 0.000     | 0.000 |
| 40 <    | 4.454     | 5.041      | 4.287      | 6.331      | 11.590         | 3.057          | 2.442      | 0.000     | 3.760 |

| Table C.10 - Example of determining the range of slope value and the value of log(pixe |
|--|
| wide x accumulation flow value)  |

| slope   | 3.4 - 3.7 | 3.7 - 3.88 | 3.88 - 4.1 | 4.1 - 4.44 | 4.44 -<br>4.72 | 4.72 -<br>5.11 | 5.11 - 5.4 | 5.4 - 5.7 | 5.7 < |
|---------|-----------|------------|------------|------------|----------------|----------------|------------|-----------|-------|
| 0 - 10  | 0.075     | 0.067      | 0.000      | 0.000      | 0.000          | 0.216          | 0.108      | 0.000     | 0.297 |
| 10 - 15 | 0.036     | 0.205      | 0.137      | 0.203      | 0.746          | 0.501          | 0.597      | 0.212     | 0.488 |
| 15 - 20 | 0.296     | 0.272      | 0.849      | 0.882      | 1.693          | 1.138          | 0.998      | 0.000     | 1.250 |
| 20 - 25 | 0.371     | 0.912      | 1.039      | 1.993      | 1.152          | 0.803          | 0.000      | 0.767     | 1.594 |
| 25 - 30 | 0.538     | 1.613      | 1.500      | 2.337      | 1.586          | 1.316          | 0.000      | 0.000     | 3.145 |
| 30 - 35 | 1.608     | 1.312      | 1.275      | 2.206      | 1.326          | 1.958          | 3.563      | 0.000     | 0.000 |
| 35 - 40 | 1.351     | 2.218      | 1.561      | 1.385      | 2.377          | 2.278          | 0.000      | 0.000     | 0.000 |
| 40 <    | 4.454     | 5.041      | 4.287      | 6.331      | 11.590         | 3.057          | 2.442      | 0.000     | 3.760 |

# Table C.11 - Example of calculation to find minimum amount of points per sub-area that most correlated with landslide occurrence

| Sub-<br>area ID | Landslide<br>occurrence | Amount of<br>landslide<br>potential points | Range amount of landslide potential points |      |       |       |       |
|-----------------|-------------------------|--|--|------|-------|-------|-------|
|                 |                         |  | 0 ≤  | 50 ≤ | 100 ≤ | 150 ≤ | 200 ≤ |
| 1               | 0                       | 0  | 1  | 0    | 0     | 0     | 0     |
| 2               | 0                       | 0  | 1  | 0    | 0     | 0     | 0     |
| 3               | 0                       | 0  | 1  | 0    | 0     | 0     | 0     |
| 4               | 0                       | 0  | 1  | 0    | 0     | 0     | 0     |
| 5               | 0                       | 0  | 1  | 0    | 0     | 0     | 0     |
| 6               | 0                       | 0  | 1  | 0    | 0     | 0     | 0     |
| 7               | 0                       | 0  | 1  | 0    | 0     | 0     | 0     |
| 8               | 0                       | 0  | 1  | 0    | 0     | 0     | 0     |
| 9               | 0                       | 0  | 1  | 0    | 0     | 0     | 0     |
| 10              | 0                       | 0  | 1  | 0    | 0     | 0     | 0     |
|                 |                         |  |  |      |       |       |       |
| 595             | 0                       | 0  | 1  | 0    | 0     | 0     | 0     |
| 596             | 0                       | 0  | 1  | 0    | 0     | 0     | 0     |
| 597             | 0                       | 0  | 1  | 0    | 0     | 0     | 0     |
| 598             | 0                       | 50   | 1  | 1    | 0     | 0     | 0     |
| 599             | 0                       | 2  | 1  | 0    | 0     | 0     | 0     |
| 600             | 0                       | 28   | 1  | 0    | 0     | 0     | 0     |
| <b>S</b> 1      | 109                     | 22435                                      |  |      |       |       |       |

|                       | 0       | 50     | 100    | 150    | 200    |
|-----------------------|---------|--------|--------|--------|--------|
| S2                    | 109     | 69     | 39     | 18     | 5      |
| \$3                   | 600     | 164    | 89     | 39     | 10     |
| Cover ratio (S2/S1)   | 100.00% | 63.30% | 35.78% | 16.51% | 4.59%  |
| Hitting ratio (S2/S3) | 18.17%  | 42.07% | 43.82% | 46.15% | 50.00% |

### Appendix D (informative) Description and interpretation technique of deep-seated landslide

For ease in interpreting the deep-seated landslide area by using imagery data, first we must know the type, shape, and character of deep-seated landslide.



Figure D.1 – The difference between shallow landslide and deep-seated landslide

As shown on Figure D.1, deep-seated landslide occurred at a depth greater than the surface landslide, so the material that is moving on deep-seated landslide is much larger than a normal surface landslide.



Figure D.2 – The shape of deep-seated landslide

The sliding surface on slip deep-seated landslide shaped like a spoon, so that when seen from above at the interpretation of image data, it looks like a curve or arc.

Here is an explanation of the interpretation and digitization techniques of deep-seated landslide area. Figure D.3 illustrates the deep-seated landslide in transverse view as well as topographic projection on a plane, or in other words that if seen from above using imagery data.



Figure D.3 – Interpretation technique of deep-seated landslide

Figure D.3 shows that there will be two types of area interpretation which are main landslide and landslide material. The area that we should to interpret is the main landslide because this part is the actual landslide location on the topography.

### Appendix E (informative) Description of micro-topographic elements

For ease in interpreting the micro-topographic elements using imagery data, first we must know the type, shape, and character of each micro-topographic elements.

There are five micro-topographic elements. As illustrated on Figure E.1, the elements are:

- 1) Ancient deep-seated landslide
- 2) Circular arc crack
- 3) Gentle ridge top
- 4) Linear depression
- 5) Mass rock creep slope



Figure E.1 – The types of micro-topographic elements

A term "scarp" as written on Figure E.1 is a line of cliffs produced by faulting or erosion; a relatively straight, clifflike face or slope of considerable linear extent, breaking the general continuity of the land by separating surfaces lying at different levels.

Figure E.2 shows the types of micro-topographic elements that are interpreted using imagery data.



Figure E.2 – The types of micro-topographic elements that interpreted on imagery data

### Appendix F (informative) Theory of Hitting Ratio and Cover Ratio

Hitting ratio and cover ratio is a statistical method to see the level of accuracy of the analysis results.

### 1) Hitting ratio

Hitting ratio can be defined as the ratio of precision, which is a way to measure the accuracy of predictive value of the presence of landslide events based on the presence of other factors in a sub-area. Hitting ratio has formula = S2/S3, where S2 is the number of sub-area that contains the element factor and has a landslide data, and S3 is the number of all sub-area that contains the element factor.

### 2) Cover ratio

Cover ratio is a way to measure the value of the coverage prediction of landslide occurrence based on the presence of other factors. Coverage ratio has formula = S2/S1, where S2 is the number of sub-area that contains the element factor and has a landslide data, and S1 is the number of sub-area that has landslide data.



Figure F.1 - The concept of hitting ratio and cover ratio theory

### Appendix G (informative) The work steps

How to find the number of landslides potential points per sub-area that are most correlated with the landslide events are as follows:

The contents of Table D.1 below comes from the example case in Sinjai region. The first column contains sub-area ID, the second column indicates whether a sub-area has landslide events, while the third column contains the number of landslide potential points per sub-area. The value of the third column is obtained through literal data of spatial data were extracted using GIS software and made into a table using spreadsheet tool software. Sub-areas with landslide events are marked in orange.

The next column is the range of landslides potential point, that is made next in the spreadsheet software tool. The columns are intended to mark the sub-areas with number of landslide potential points according to a certain amount by multiples of fifty.

| Sub-area<br>ID | Landslide<br>events | Number of landslide<br>potential points | The range of number of landslide potential points |      |       |       |       |
|----------------|---------------------|---|---|------|-------|-------|-------|
|                |                     |   | 0 ≤   | 50 ≤ | 100 ≤ | 150 ≤ | 200 ≤ |
| 1              | 0                   | 156                                     | 1   | 1    | 1     | 1     | 0     |
| 2              | 0                   | 112                                     | 1   | 1    | 1     | 0     | 0     |
| 3              | 0                   | 62                                      | 1   | 1    | 0     | 0     | 0     |
| 4              | 0                   | 135                                     | 1   | 1    | 1     | 0     | 0     |
| 5              | 0                   | 78                                      | 1   | 1    | 0     | 0     | 0     |
| 6              | 0                   | 107                                     | 1   | 1    | 1     | 0     | 0     |
| 7              | 1                   | 53                                      | 1   | 1    | 0     | 0     | 0     |
| 8              | 0                   | 115                                     | 1   | 1    | 1     | 0     | 0     |
| 9              | 0                   | 49                                      | 1   | 0    | 0     | 0     | 0     |
| 10             | 0                   | 12                                      | 1   | 0    | 0     | 0     | 0     |
| 11             | 1                   | 128                                     | 1   | 1    | 1     | 0     | 0     |
| 12             | 0                   | 64                                      | 1   | 1    | 0     | 0     | 0     |
| 13             | 0                   | 92                                      | 1   | 1    | 0     | 0     | 0     |
| 14             | 1                   | 149                                     | 1   | 1    | 1     | 0     | 0     |
| 15             | 0                   | 4                                       | 1   | 0    | 0     | 0     | 0     |
| 16             | 0                   | 109                                     | 1   | 1    | 1     | 0     | 0     |
| 17             | 0                   | 100                                     | 1   | 1    | 1     | 0     | 0     |
| 18             | 0                   | 48                                      | 1   | 0    | 0     | 0     | 0     |
| 19             | 0                   | 74                                      | 1   | 1    | 0     | 0     | 0     |
| 20             | 0                   | 151                                     | 1   | 1    | 1     | 1     | 0     |
| 21             | 0                   | 70                                      | 1   | 1    | 0     | 0     | 0     |
| 22             | 0                   | 65                                      | 1   | 1    | 0     | 0     | 0     |
| 23             | 0                   | 82                                      | 1   | 1    | 0     | 0     | 0     |
| 24             | 0                   | 15                                      | 1   | 0    | 0     | 0     | 0     |
| 25             | 0                   | 95                                      | 1   | 1    | 0     | 0     | 0     |
| 26             | 0                   | 44                                      | 1   | 0    | 0     | 0     | 0     |
| 27             | 0                   | 77                                      | 1   | 1    | 0     | 0     | 0     |
| 28             | 0                   | 108                                     | 1   | 1    | 1     | 0     | 0     |
| 29             | 1                   | 211                                     | 1   | 1    | 1     | 1     | 1     |
| 30             | 0                   | 62                                      | 1   | 1    | 0     | 0     | 0     |
| 31             | 0                   | 126                                     | 1   | 1    | 1     | 0     | 0     |
| 32             | 0                   | 3                                       | 1   | 0    | 0     | 0     | 0     |
| 33             | 0                   | 38                                      | 1   | 0    | 0     | 0     | 0     |
| 34             | 0                   | 115                                     | 1   | 1    | 1     | 0     | 0     |
| 35             | 0                   | 217                                     | 1   | 1    | 1     | 1     | 1     |
| 36             | 0                   | 52                                      | 1   | 1    | 0     | 0     | 0     |
| 37             | 0                   | 94                                      | 1   | 1    | 0     | 0     | 0     |
| 38             | 0                   | 20                                      | 1   | 0    | 0     | 0     | 0     |

# Table G.1 – The calculation table of the number of landslide potential point that correlates with landslide events per sub-area

| 39       | 0 | 70  | 1   | 1 | 0 | 0 | 0 |
|----------|---|-----|-----|---|---|---|---|
| 40       | 1 | 195 | 1   | 1 | 1 | 1 | 0 |
| 41       | 0 | 94  | 1   | 1 | 0 | 0 | 0 |
| 42       | 0 | 158 | 1   | 1 | 1 | 1 | 0 |
| /3       | 0 | 130 | 1   | 1 | 1 | 0 | 0 |
| 43       | 0 | 05  | 1   | 1 | 0 | 0 | 0 |
| 44       | 1 | 01  | 1   | 1 | 0 | 0 | 0 |
| 45       | 1 | 91  | 1   | 1 | 0 | 0 | 0 |
| 40       | 0 | 37  | 1   | 0 | 0 | 0 | 0 |
| 47       | 0 | 13  | 1   | 0 | 0 | 0 | 0 |
| 48       | 1 | 144 | 1   | 1 | 1 | 0 | 0 |
| 49       | 0 | 124 | 1   | 1 | 1 | 0 | 0 |
| 50       | 0 | 110 | 1   | 1 | 1 | 0 | 0 |
| 51       | 1 | /3  | 1   | 1 | 0 | 0 | 0 |
| 52       | 0 | 53  | 1   | 1 | 0 | 0 | 0 |
| 53       | 0 | 85  | 1   | 1 | 0 | 0 | 0 |
| 54       | 1 | 129 | 1   | 1 | 1 | 0 | 0 |
| 55       | 1 | 136 | 1   | 1 | 1 | 0 | 0 |
| 56       | 1 | 87  | 1   | 1 | 0 | 0 | 0 |
| 57       | 1 | 105 | 1   | 1 | 1 | 0 | 0 |
| 58       | 1 | 113 | 1   | 1 | 1 | 0 | 0 |
| 59       | 1 | 174 | 1   | 1 | 1 | 1 | 0 |
| 60       | 0 | 80  | 1   | 1 | 0 | 0 | 0 |
| 61       | 0 | 116 | 1   | 1 | 1 | 0 | 0 |
| 62       | 1 | 88  | 1   | 1 | 0 | 0 | 0 |
| 63       | 0 | 38  | 1   | 0 | 0 | 0 | 0 |
| 64       | 0 | 53  | 1   | 1 | 0 | 0 | 0 |
| 65       | 1 | 134 | 1   | 1 | 1 | 0 | 0 |
| 66       | 0 | 20  | 1   | 0 | 0 | 0 | 0 |
| 67       | 1 | 120 | 1   | 1 | 1 | 0 | 0 |
| 68       | 1 | 153 | 1   | 1 | 1 | 1 | 0 |
| 69       | 0 | 61  | 1   | 1 | 0 | 0 | 0 |
| 70       | 1 | 82  | 1   | 1 | 0 | 0 | 0 |
| 71       | 0 | 26  | 1   | 0 | 0 | 0 | 0 |
| 72       | 0 | 85  | 1   | 1 | 0 | 0 | 0 |
| 73       | 0 | 165 | 1   | 1 | 1 | 1 | 0 |
| 74       | 0 | 97  | 1   | 1 | 0 | 0 | 0 |
| 75       | 0 | 42  | 1   | 0 | 0 | 0 | 0 |
| 76       | 0 | 195 | - 1 | 1 | 1 | 1 | 0 |
| 77       | 0 | 194 | 1   | 1 | 1 | 1 | 0 |
| 78       | 0 | 118 | 1   | 1 | 1 | 0 | 0 |
| 79       | 0 | 152 | 1   | 1 | 1 | 1 | 0 |
| 80       | 0 | 83  | 1   | 1 | 0 | 0 | 0 |
| 81       | 0 | 134 | 1   | 1 | 1 | 0 | 0 |
| 82       | 0 | 110 | 1   | 1 | 1 | 0 | 0 |
| 82       | 0 | 20  | 1   | 1 | 0 | 0 | 0 |
| 8/       | 0 | 25  | 1   | 0 | 0 | 0 | 0 |
| 04<br>QE | 0 | 57  | 1   | 1 | 0 | 0 | 0 |
| 86       | 0 | 15  | 1   | 0 | 0 | 0 | 0 |
| 00       | 0 | 101 | 1   | 1 | 1 | 1 | 0 |
| 0/       | 0 | 217 | 1   | 1 | 1 | 1 | 1 |
| 00       | 0 | 100 | 1   | 1 | 1 |   |   |
| 00       | 0 | 140 | 1   | 1 | 1 | 0 | 0 |
| 90       | 0 | 142 | 1   | 1 | 1 | 0 | 0 |
| 91       | 0 | 00  | 1   | 1 | 0 | 0 | 0 |
| 92       | 1 | 109 |     | 1 |   |   | 0 |
| 93       | 0 | 231 | 1   | 1 | 1 | T | 1 |

Max Value

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|                       | 0       | 50      | 100    | 150    | 200    |
|-----------------------|---------|---------|--------|--------|--------|
| S2                    | 20      | 20      | 14     | 5      | 1      |
| S3                    | 93      | 76      | 43     | 16     | 4      |
| Cover ratio (S2/S1)   | 100.00% | 100.00% | 70.00% | 25.00% | 5.00%  |
| Hitting ratio (S2/S3) | 21.51%  | 26.32%  | 32.56% | 31.25% | 25.00% |
|                       | 21.51%  | 26.32%  | 22.79% | 7.81%  | 1.25%  |

To find a correlation of number of landslide potential points with landslide events, hitting ratio and cover ratio method is used. The number of values in the second column is the value for the parameter of S1 which is the number of sub-areas contained landslide events. In the above column, the value of S1 is 20. The number of values in the fourth, fifth, sixth, seventh and eighth column are the parameters of S3 for each number parameter of multiple 50.

Parameter S2 is the number of sub-areas with landslide events as well as parameter of specific number of factors. For example, in the fourth column for the number parameter 0, the value of S2 is 20; in the fifth column for the number parameter 50, the value of S2 is 20; in the third column for the number parameter 100, the value of S2 is 14; so on.



Figure G.1 – The calculation result of hitting ratio and cover ratio

After obtaining all the values for the parameters S1, S2, and S3, next is to calculate the value of hitting ratio and cover ratio. These values are calculated on a small column at the bottom. From the calculation is known that the fifth column is the column that shows the number of landslide potential points per sub-area or at least 50 which is the most correlated with the landslides occurrence.

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